

FNAL Site No/	Div. Specific No.	<b>154</b>	Asset No.
If applicable	If applicable		If applicable

Device Name or Description	Coil Insert Lifting Fixture for SM3 Disassembly & VM Assembly
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Engineering Note Prepared by	<u>Edward Chi</u>	Date	<u>January 28, 2005</u>
Engineering Note Reviewed by	<b>Dave Pushka</b>	Date	

Capacity	<b>6,500 lbs.</b>
Fixture Weight	<b>180 lbs.</b>

### Inspections Frequency

Signature (of Load Test Witness)

See page 8 for rated load test procedures;  
page 9 for rated load test setup layout;  
page 10 for rated load test site pictures if have any.



Fermilab

## **Particle Physics Division Mechanical Department Engineering Note**

Number: MD-ENG- 073

Date: January 28, 2005

Project Internal Reference:

Project: BTeV, SMTF

Title: Coil Insert Lifting Fixture for SM3 Disassembly & VM Assembly

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Reviewer(s): David Pushka

Key Words: Coil, insert lifting fixture, tubing, threaded rod, axial allowable stresses, critical force, buckling.

### **Abstract Summary:**

The insert lifting fixture is specially designed to lift the sm3 & VM coil (inner, middle and outer coil) vertically from the limited accessed space area, and then move to the designated location. The working stresses of fixture structure; the buckling behavior of the slim tubing with threaded rod; the welding sizes of the lifting lug have been presented for discussion and calculation per the related industrial specifications and codes.

### **Applicable Codes:**

“Allowable Stress Design”, AISC, 9<sup>th</sup> edition

“Below-the-Hook Lifting Devices”, ASME B30.20

“Structural Welding Code-Steel”, AWS D1.1-90

“Steel structures Design and Behavior” by C. Salmon & J. Johnson, 3<sup>rd</sup> edition, 1990

## Design the Coil lifting Turning Fixture for SM3 & VM Magnets

### Design Criteria and Assumptions:

Total design load:

Lifting capacity:  $P_{c1} = P_{c2} = 13,000 \text{ lbs} / 2 = 6,500 \text{ lbs.}$

Fixture weight  $W_d = 180 \text{ lbs.}$  (dead weight)

Gross force to the fixture:  $P_{ty} = 6,500 \text{ lbs} + 180 \text{ lbs.} = 6,680 \text{ lbs.}$

All plates: ASTM A36:  $F_u = 58 \text{ ksi}$ ,  $F_y = 36 \text{ ksi}$

All tubings: Carbon stl. AISI 1020,  $F_u = 52 \text{ ksi}$ ,  $F_y = 38 \text{ ksi}$

All bolt materials: Grade 5 steel,  $F_u = 120 \text{ ksi}$

All weld materials: E70, where  $F_u = 70 \text{ ksi}$

### Reference Drawings:

LE- 407840, MC-407784, MB-407790, MB-407786, MB-407787, MB-407788

### The application of the coil insert lifting fixture:

The coil insert lifting fixture specially designed: lift & move the coil away from the limited access space area as shown on figure 10 of dwg. LE-407840; and then move the coil to the designated area for installing the coil turning fixture as shown on figures 11a to 11c of drawing LE-407840.

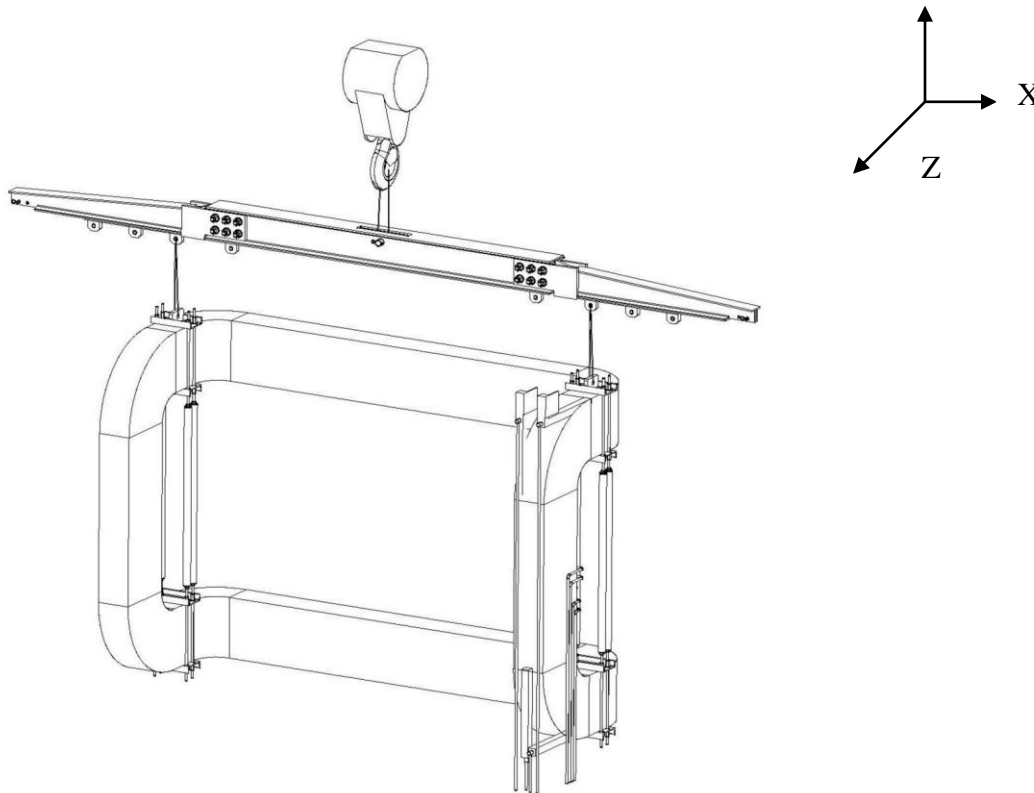


Figure 1. Using the coil insert lifting fixture to lift the coil vertically

Figure 1 on page 3 shown the application of the coil insert lifting fixture: two coil insert lifting fixtures lifted the coil through the coil lifting spreader bar. It is assumed that there is about 6,680 lbs force ( $P_{ty}$ ) applying to each coil insert lifting fixture.

Figure 2 is the detail engineering drawing of the coil insert lifting fixture, the coil was supported by upper and bottom decks, there are (4) tubes with threaded rods connected upper and bottom decks together as shown on drawing MC-407784.

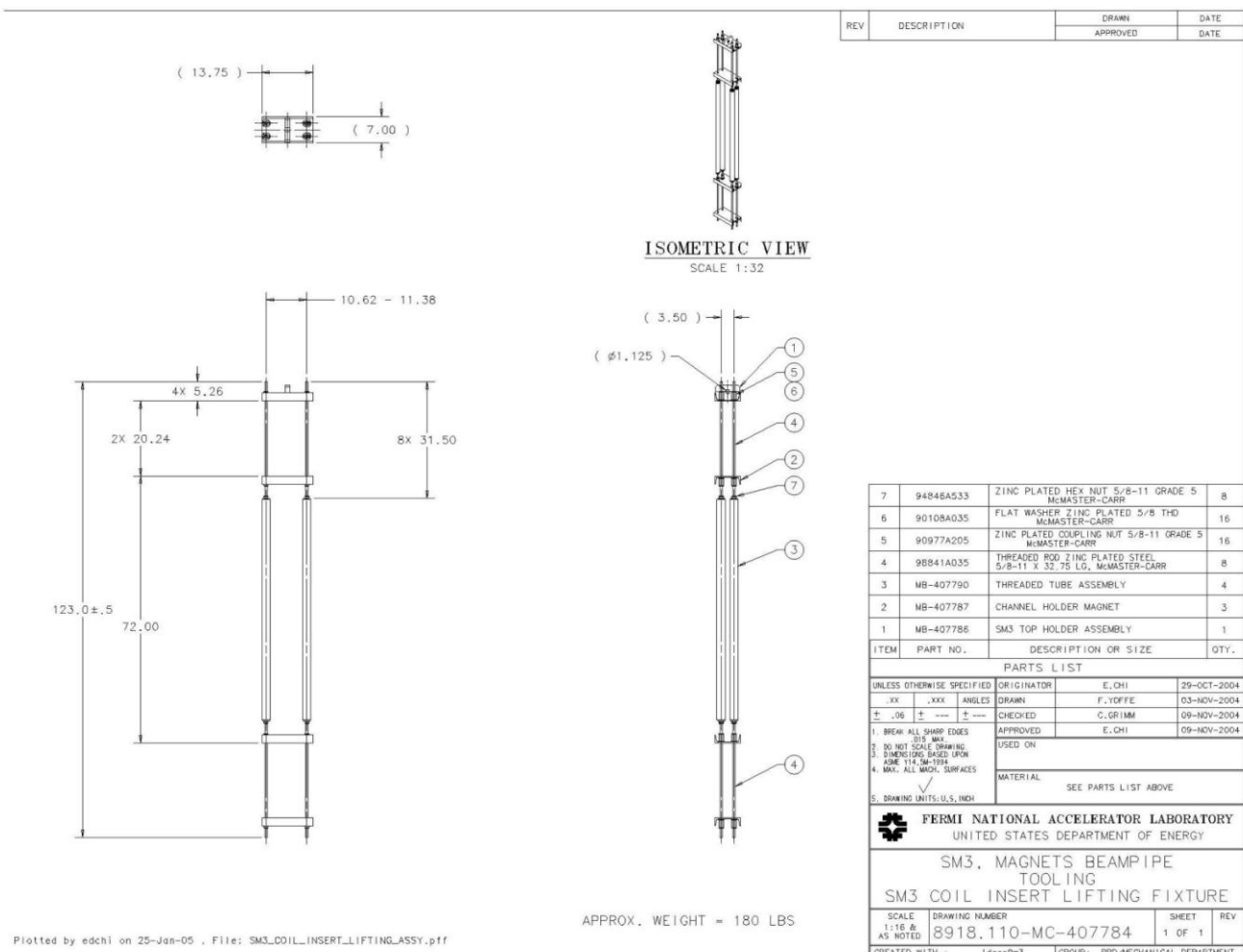


Figure 2. The detail eng. drawing of the coil insert lifting fixture.

### I. *The discussion of the load condition of the coil insert lifting fixture.*

When coil is lifted by the coil insert lifting fixture, it is assuming that the tube with threaded rod mainly subjected two forces: tension load and compressive load

a) Discuss the working tensional load  $p_{tr}$  of the threaded rod:

Conservatively assuming that one rod takes whole load  $p_t = 6,680 \text{ lbs.} = p_{tr}$

The specifications of the threaded rod: grade 5 steel, 5/8" – 11, UNC,

$$F_u = 120 \text{ ksi},$$

$$F_t = 0.33 F_u = 39.6 \text{ ksi}, \text{ the allowable tensile stress of the threaded rod}$$

(per page 4-3, part 4 of ASD, 9<sup>th</sup> edition)

$$P_t = \text{Gross area of the threaded rod} \times \text{allowable tensile stress}$$

$$= 0.3068 \text{ in}^2 \times 39.6 \text{ ksi}$$

$$= 12.15 \text{ kip} > p_t = 6.680 \text{ kip} = p_{tr}$$

where  $P_t$  is the allowable tensional load for the thread of 5/8" nominal diameter.

**The designated threaded rod has enough capacity to take the subjected tensional load.**

b). *Discuss the work condition of the tube with threaded rod subject the axial load  $P_{ca}$ .*

$$P_{ca} = P_{ty} / n, \quad \text{compressive axial load per tubing column}$$

$$= 6,680 \text{ lbs} / 4 = 1.67 \text{ kip},$$

$n$ : number of the tubing columns per insert lifting fixture

b1). Find out the critical force  $P_{cr}$  to cause the column to buckling:

$$\begin{aligned} P_{cr} &= (\Pi^2 E) A_g / (KL/r)^2 \\ &= [(\Pi^2 \times 29 \times 10^6 \text{ ksi}) \times 1.215 \text{ in}^2] \div (2.0 \times 72.0 \text{ in} / 0.732 \text{ in})^2 \\ &= 8.986 \text{ kip} > P_{ca} = 1.67 \text{ kip} \end{aligned}$$

(see section 6.3, Steel Structures Design & Behavior, 3<sup>rd</sup> edition)

**So there is no buckling under the current load conditions.**

where:  $E = 29 \times 10^6 \text{ ksi}$ , modulus of elasticity of the subjected member

$A_g = 1.215 \text{ in}^2$ , for gross cross-section area of the tubing with 2.25" od. and 3/16" wall thickness (see drawing MB-407790 for ref.)

$L = 72.0 \text{ in}$ , the length of the subjected member conservatively assumed.

$K = 2.0$ , assuming effective length factor

$I = 0.651 \text{ in}^4$ , geometrical inertia of the tubing.

$r = 0.732 \text{ in}$ , radius of gyration

b2). Find out the allowable stresses vs. the computed working stresses:

$$\begin{aligned} F_{a1} &= 12 \Pi^2 E \div 23 (KL/r)^2 \\ &= (12 \Pi^2 \times 29,000 \text{ ksi}) \div 23 \times 196.7^2 \\ &= 3.86 \text{ ksi} \end{aligned}$$

(see eq. E2-2, Chapter E, Part 5, ASD, 9<sup>th</sup> edition)

where:  $F_{ai}$ : the allowable axial stress for the compressive member

$KL/r = 2.0 \times 72 \text{ in} / 0.732 \text{ in} = 196.7$ , the largest effective slenderness ratio

$$C_c = [(2 \Pi^2 E) / F_y]^{1/2} = 122.73 < KL/r = 196.7$$

$F_y = 38$  ksi, yielding stress for tubing with AISI 1020, carbon stl.  
per section 20-1.2.2.2, ASME B30.20

$$F_b = F_y / 3.0 = 12.67 \text{ ksi} = F_v = F_{a2}$$

Pick the less value one as allowable stress,

so  $F_a = 3.86$  ksi.

$$\begin{aligned} f_a &= P_c / A_g = 1,670 \text{ lbs} / 1.215 \text{ in}^2 \\ &= 1.375 \text{ ksi} < F_a = 3.86 \text{ ksi}, \end{aligned}$$

**The computed axial working stress is satisfactory subjecting the axial applying force.**

### 3. Weld Calculations:

The figure 3 is the weld configuration for the lifting lug of the coil insert lifting fixture,  
See drawings MB-407788, MB-407786 and MC-407784 for the reference.

Find the geometrical properties of the welds as shown on figure 3:

Where:  $d = 1.25$  inch,

$b = 5.0$  inch

$L = 2b = 10$  in, length of the welds

$$\begin{aligned} I_{xx} &= bd^2 / 2 \\ &= 3.9 \text{ in}^3 \end{aligned}$$

$$\begin{aligned} S_{xx} &= bd \\ &= 6.255 \text{ in}^2 \end{aligned}$$

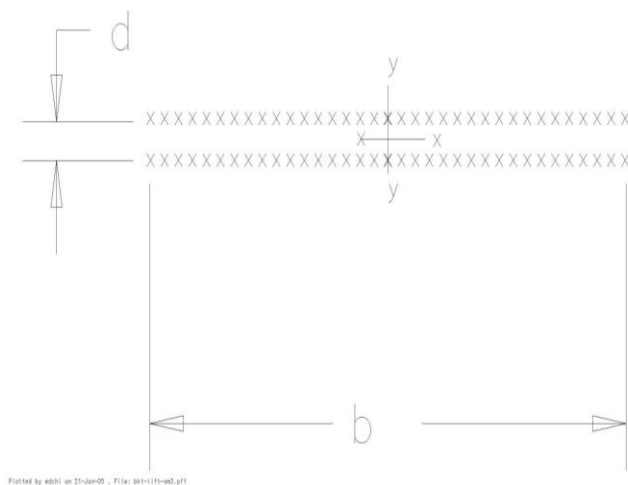


Figure 3. The weld configuration for the lifting lug of the coil insert lifting fixture (treat as line with unit thickness).

The working load per unit length of the weld subject to the applying load can be found:

$$\begin{aligned}f_v &= P_{ty} / L \\&= 6.680 \text{ lbs} \div 10 \text{ in} \\&= 668 \text{ lbs/in}\end{aligned}$$

Per figure 1 for the application of the insert lifting fixture, it can be assumed that there is no significant moment to be produced from the subjected applying load.

$$\begin{aligned}\text{So: } f_r &= f_v \\&= 668 \text{ lbs/in}\end{aligned}$$

where:  $f_r$  is the combined working load per unit length

To find the required weld size  $C_I$ :

All weld metals are E70,

Where:  $F_u = 70 \text{ ksi}$

The allowable stresses for the weld metals:

$$F_t = F_v = 0.30 F_u = 21 \text{ ksi}$$

$$\begin{aligned}C &= \text{combined working load per unit length} \div (\text{effective factor} \times \text{allowable stress}) \\&= (668 \text{ lbs/in}) \div (0.707 \times 21 \text{ ksi}) \\&= 0.045 \text{ in} < 0.31 \text{ in (the designated weld size in the area per drawing MB-407786)}\end{aligned}$$

**The designated weld sizes are satisfactory.**

### ***Conclusions:***

The coil insert lifting fixture has been designed per the related engineering codes after the discussions from several different areas, such discussions were presented by computing the working structural stresses; allowable axial stresses of the slim tubing column; and finally the weld sizes in terms the different applications.

## **Rated Load Test Procedures for SM3 Coil Insert Lifting Fixture**

1. Review the load test setup on figure 4 of page 9 and the lifting fixture engineering drawing MC-407784, call Edward Chi @x2879 for the questions.
2. Prepare and move the items to the designated area:
  - a). Three B shield blocks
  - b). Two existing steel tubes:  
One with sizes of 10" x 12" x ½" with 10' in length,  
Another one with sizes of 10" x 10" x ½" x 120".
  - c). Two timber blocks:  
One with one sizes of 8" x 8" x 24"  
Another one with sizes of 10" x 8" x 24"
  - d). 8 pieces of garden hose (~19" in length) – or equivalent, for threaded rod protections.
  - e). 8 pieces of steel angles or equivalent parts for restricting the sling contact area
  - f). Slings with spec. as shown on figure 4.
  - g). Hoist scale
  - f). One 1" dia, alloy steel anchor shackle
3. Assemble all items per load test set up as shown on figure 4 of page 9 (per right side view), uniformly apply the clamping force to the tubes and blocks through the threaded rods, the tight torque to the nut is about 75 ft-lbs. Cross-check the position per the test setup layout and drawing MC-407784.
4. Lift up the assembled test fixture slowly, apply the slings per the test setup on figure 4 (see the front view), make sure that both slings stay on the distance of 30" and 60" as shown on the front view of figure 4.
5. Gradually, slowly apply load through crane until the scale reading reaches 8,350 lbs, sustain such load up to 10 minutes, observe the fixture to see if there is any irregular mechanical behavior.
6. Take the pictures for the load test setup.
7. Fill out and sign the form 5022.1TA (page 1) as Load Test Witness
8. Remove every item back in order.
9. Mark the fixture as:  
Number 154  
Lifting Capacity: 6,500 lbs.  
Fixture weight: 180 lbs.
10. Thanks for finish the project safely and successfully.



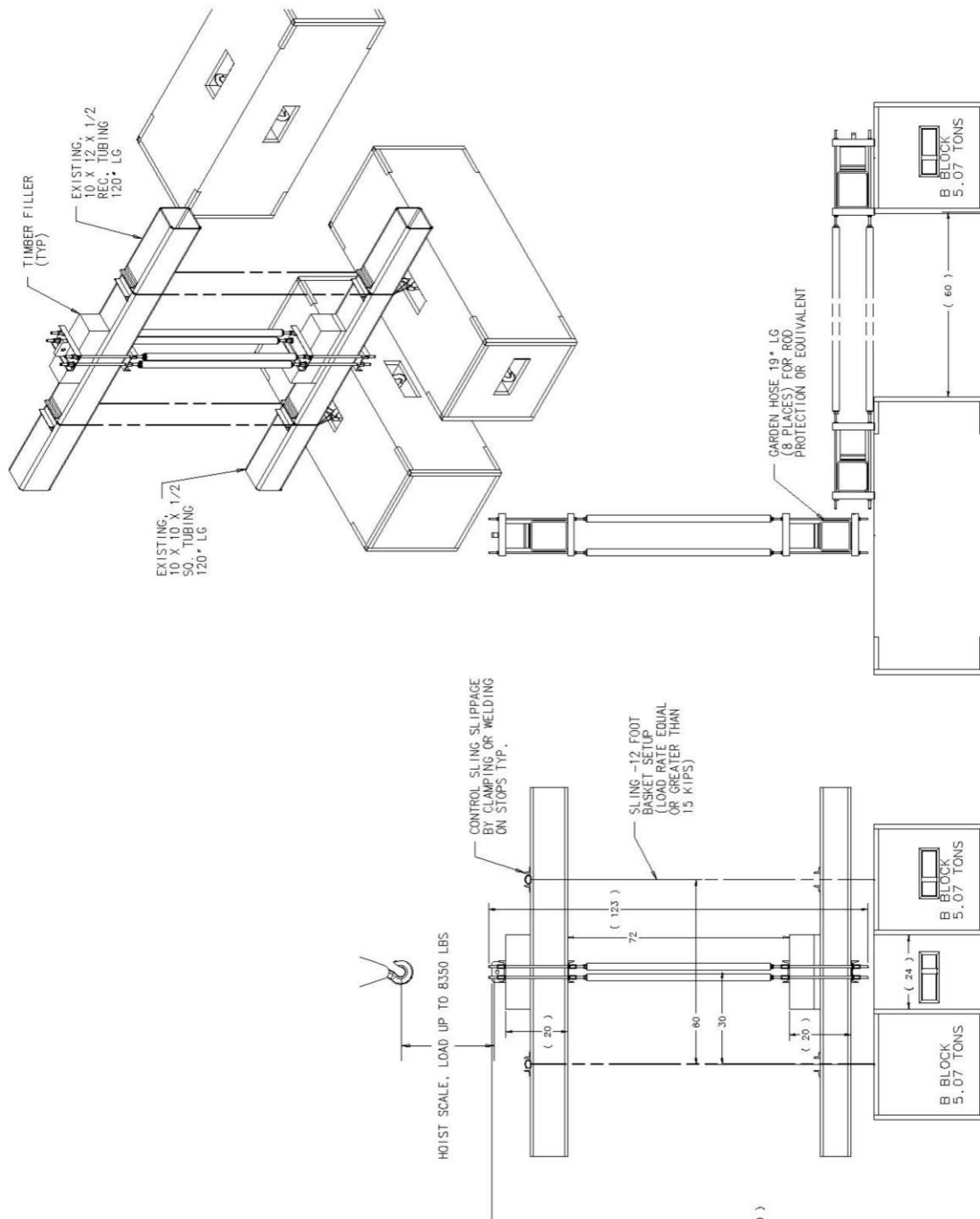


Figure 4. SM3 Coil Insert Lifting Fixture Load Test Setup

